

## Reprocessed Materials Evaluation on Perfunctory and Flame Endurance of Structures

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### Abstract

The fire resistance of concrete with low fire resistance and meagre fire resistance can be improved by replacing the cement in the concrete mixture with different GGBS ratios. By partially substituting cement with GGBS (ground blast furnace slag), which can be used as an additive to assure excellent heat resistance in concrete, the GGBS can help lower the price of concrete mixtures, prevent concrete from cracking, reduce high temperatures and increase compressive strength. For OPC concrete mixtures, the exact optimal cement substitution rate of GGBS (15-60%, in steps of 15%) must be reached for mechanical (compressive strength, tensile strength and flexural strength) analysis, durability (constant pressure and water absorption), GGBS concrete mixture mass loss due to acid attack and microstructure characteristics (FESEM and FTIR), assuming a water-cement ratio of 0.4. (Mixture 1 with 100% and Mixture 2 with the best GGBS percentage) After exposure to the flame, the resistance is calculated. Curing HSC performance is observed under the influence of thermal annealing. Higher temperature is observed in various mixtures and densities.

**Keywords:** Cement, GGBS, Mechanical performance, Microstructural analysis, High strength concrete, Temperature

### 1. Introduction

Concrete is a standout among the maximum standard improvement cloth withinside the slicing part global. It is applied to bind different shape substances collectively. Concrete has made global slicing a possibility. It supports the world's tallest buildings, as well as metros, roadways, and interstates. It also helps spans, burrows, dams, and trenches, as well as schools, universities, and medical clinics. Concrete is the most important large-scale cloth product in the manufacturing industry. On the occasion that cement's embodied electricity may fade without growing, the financial and fee benefits are probably reckoned. Despite the fact that concrete is a fire-resistant building

material, when a fire occurs, the temperature is increased by a significant amount. At those temperatures, concrete loses its mechanical residences consisting of power, stiffness, etc., Also, it undergoes spalling and shrinkage. It has been accounted for that the manufacturing of 1 ton of Portland cement might require kind of 1.5 heaps of mineral extractions together with 5000 MJ of electricity, 0.95 tonnes of CO<sub>2</sub> might be produced proportionally. GGBS is a spinoff of the iron industry, and it has been calculated that 1 tonne of GGBS would produce roughly 0.07 tonnes of CO<sub>2</sub> equivalent and consume just around 1300 MJ of power (Saklecha, Kedar, & Professor, 2015). The use of GGBS instead of Portland cement will set

off a massive lower carbon dioxide fuel online outflow. In India, we produce approximately 7.8 million heaps of GGBS. The disposal of such slag while a waste fill is trouble and might motive true herbal perils with the industry's predicted financial improvement and development. A part of the continuing investigations in one-of-a-kind global portions has exposed that GGBS may be proficiently applied as a fine cementitious constituent in cement. It has also tested its flexibility and durability in using systems altogether, helping the visionary implement affordable improvement. When applied in cement, GGBS is a cementitious material that could move approximately as a partial substitution for Portland cement deprived of buying and selling off the compressive power. Workability, durability, and quality are all important factors to consider. Several searches revealed the deterioration of concrete compressive strength under high-temperature exposure. On this inquiry, an attempt was made to look into temperature grade affect and exposure to fiery-warm blazes on high-power concrete mechanical residences. Rao, Sravana, and Rao (2016) proposed a lower mechanical power for GGBS percentage at three days (10-60 percent at an increment of 10 %). It did, however, demonstrate significant development after that. At 7, 28, and 90 days, the increase in compressive strength was approximately 22.6 %, 4.5 %, and 17.7 %, respectively. A suitable amount of flexural strength development is also observed. At 7, 28, and 90 days, the increase became 6.25 %, 16.17 %, and 13.9 %, respectively, which is a long time. At 7, 28, and 90 days, the increase in cut-up tensile power was approximately 29.4 %, 50.4 %, and 72.2 %, respectively. The most appropriate replacement acquired became 40%. This growth is probably because of the pozzolanic reaction, which became more excellent solid later as he accomplished [1]. Ganesh & Murthy (2019) found significant growth in compressive power with growth in GGBS content material as much as 40% and 20 % while well-known water curing and expanded temperature curing are provided, respectively. He also found that because of the slower hydration process, early age compressive strength is not typically addressed; temperature curing complements the hydration process, resulting in faster power achievement [2].

Several techniques in favour of worsened concrete owing to high heats have been documented, including positive mixture segment alteration, and microcracks proliferation owing to thermal unsuitability amongst cement and mixture segment [3-8]. Umran looked at the impact of fireplace advertising on concrete homes. Temperature intensities of 400°C, 500°C, and 700°C were chosen, as well as four different exposure times ranging from 30 minutes to 2 hours with a 0.5-hour increment also the ultrasonic pulse pace and dynamic modulus of elasticity have been measured [9,10].

## 2. Methodology

### 2.1 Experimental Programme

The experiment was carried out to determine the heat range and burning period. Mathematical models were planned to predict concrete strengths when exposed to fireplace flame thanks to various tests like compressive, tensile, and flexural strengths. 100 x 100 x 100mm cubes, 100mm diameter 200mm long cylinders, and 100 x 100 x 500mm beams were forged as specimens to test compressive, flexural, and split tensile strengths, respectively, according to IS [11]. Beams, cubes and cylinders specimen are shown in Fig. 1.

Various new solidified concrete details of many testing have been handed. All strengths, such as tensile, flexural and compressive, were determined for each concrete mix by taking the average of three specimens with a consistent natural process period. Strength was measured after 7, 28, and 90 days of cure.



**Fig.1. Beams, cubes and cylinders sample**

HSC samples were set ablaze with direct fiery-hot flames by methane-burners web amidst a stockpile of bricks with dimensions of 800 x 800 x 1000mm in height.

**2.2 Material and Mixture preparation**

**Table.1. Cement configuration**

Oxide	%	Standard limits
SiO <sub>2</sub>	20.0	
CaO	61.2	
Fe <sub>2</sub> O <sub>3</sub>	3.5	
Al <sub>2</sub> O <sub>3</sub>	6.4	
SO <sub>3</sub>	2.2	≤ 2.8
MgO	4.1	≤ 0.5
IR	0.5	≤ 1.5
LOI	1.5	≤ 4.0
Excess lime	0.6	
Bough's Compound	%	
C <sub>3</sub> S	38.95	
C <sub>2</sub> S	29.98	
C <sub>3</sub> A	12.87	
C <sub>4</sub> AF	8.37	

**Table.2. Cement physical properties**

S. No	Physical-properties	Apparatus	Test results	IS: 1984 limits
1.	setting time Initial Final	Vicat's apparatus	1 hrs. 40 min. 3 hrs. 60 min.	≥ 1 hr. ≤ 10 hrs.
2.	Fineness	Blaine's apparatus	3180 cm <sup>2</sup> /g m.	≥ 2300 cm <sup>2</sup> /g m.
3.	Compressive strength (cement mortar 70.6mm cube size) 3 days 7 days	Compression Testing Machine (CTM)	24 MPa 29 MPa	≥ 15 MPa ≥ 23 MPa

Ordinary portland cement (OPC) made at the Kufa manufactory is employed in this study. This cement met Iraqi Specification No. 5 requirements (1984). Table 1 and Table 2 list the chemical constituents and physical attributes. As a rough and acceptable aggregate component, crushed volcanic rock having specific gravity of 2.65 with a maximum combined size of 10 mm and river sand having specific gravity of 2.62 were employed.

The native seller procured the furnace waste slag having specific gravity of 2.69 from Gujarat. This waste slag was subjected to a relative density test. At a constant water/cement ratio of 0.4, four following concrete mixes including blast furnace slag are created. To obtain the optimum quantity for replacement, BF slag was substituted for cement in quantities in four proportions of 0 to 60% at an increment of 15% (as shown in Table 3).

**Table.3. GGBS mix quantities in kg/m<sup>3</sup>**

GGB S (%)	Cement (kg/m <sup>3</sup> )	Fine aggregate (kg/m <sup>3</sup> )	Coarse aggregate (kg/m <sup>3</sup> )	Admixturer (%)
0	386	640.76	1317.03	0.1
15	328.1	640.76	1317.03	0.1
30	270.2	640.76	1317.03	0.1
45	212.3	640.76	1317.03	0.1
60	154.4	640.76	1317.03	0.1

After getting an optimum quantity of GGBS, two mixes were investigated; mix 1 consisted of 535 Kg/m<sup>3</sup> of cement. In mix 2, 45% GGBS (obtained as optimum) and 55% cement (O.P.C) (GGBS was replaced from cement). For all mixes, constant dosage of superplasticizers and the water to cement ratio were kept 1.0 % and 0.40 by weight of cement.

Experiments were carried out to determine the heat intensity and duration of fiery-hot. Temperatures of 400, 600, and 850°C were chosen as the highest fire flame exposure limits. The fire flame revelation period was chosen as 2 hours to protect the extent of scenarios of better heat trial in the greater portion.

### 3. Results and Discussions

#### 3.1 GGBS and Cement

The cement particles have uneven outlines, according to the FESEM investigation. The GGBS particles, on the other hand, are angular at different magnifications, as illustrated in Fig. 3. The composition of the elements contained in the material is shown in Fig. 2 by the EDAX analysis. Table 4 shows the elemental compositions of cement and GGBS. Higher component values are determined by high-intensity peaks.

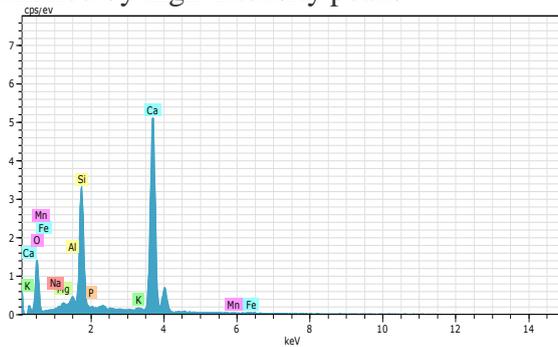


Fig. 2. Cement EDAX analysis

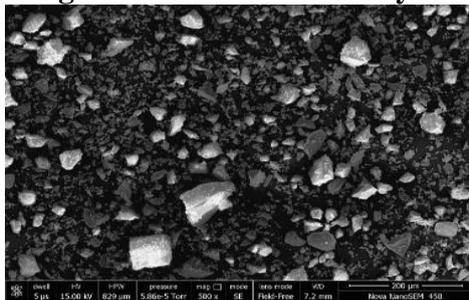


Fig. 3. GGBS FESEM analysis image

#### 3.2 Fine aggregate

Fine aggregate FESEM study depicts the smooth texture and uneven shape of fine aggregate as seen in Fig. 4(a). According to the EDAX study shown in Fig. 4(b), oxygen and silica had the highest fractions.

Table.4. Primary composition of GGBS and cement

GGBS			Cement	
Elements	Symbol	%	Oxides	%
Silica	Si	24.78	SiO <sub>2</sub>	21.70
Aluminum	Al	3.69	Al <sub>2</sub> O <sub>3</sub>	5.18
Iron	Fe	2.28	Fe <sub>2</sub> O <sub>3</sub>	3.78
Calcium	Ca	66.0	CaO	62.93
Potassium	K	0.51	MgO	2.55
Magnesium	Mg	2.80	SO <sub>3</sub>	2.71
Sodium	Na	0.08	K <sub>2</sub> O,	0.90,
			Na <sub>2</sub> O <sub>3</sub>	0.26

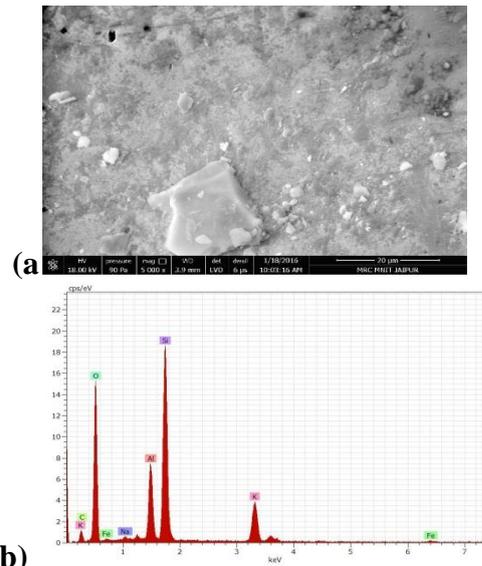


Fig. 4. (a) fine aggregate FESEM analysis image (b) fine aggregate EDAX analysis

#### 3.3 Bulk density and Workability

To measure the density of cubes first external surface of the cube is cleaned and wiped with the help of any cotton cloth. Fig. 5 shows the apparent density of the GGBS concrete mixture. The bulk density of the freshly mixed concrete mixture decreases as the percentage of GGBS increases. For GG1, GG2, GG3 and GG4 decrements are 0.17%, 0.38%, 0.43% and 0.57%.

Because the specific gravity of GGBS is 2.69, which is lower than that of cement, the decrease in the bulk density of fresh materials could be due to this. In Table 5, the percentage of superplasticizers used in concrete mixtures has been rigorously tested so that the compaction coefficient is zero.

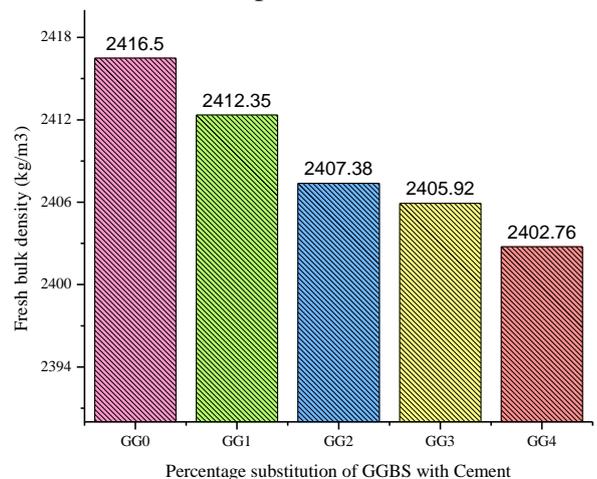


Fig. 5. GGBS samples Fresh density

**Table.5. Workability of GGBS mixes**

Mix No.	Admixture (%)	Compaction factor
GG0	0.10	0.90
GG1	0.12	0.90
GG2	0.14	0.90
GG3	0.16	0.90
GG4	0.18	0.90

**3.4 Compressive strength**

The compressive strength trends of GGBS after 7 and 28 days are shown in Fig. 6. After 7 and 28 days, an increase in compressive strength was observed due to the partial replacement of cement by GGBS (15-60%, an increase of 15%). Up to 45 percent (GG3) replacement cement showed good compressive strength for a total of 60 percent GGBS replacement. Compressive strength tests after 7 and 28 days revealed the best mixing effect when 45% GGBS was used instead of cement. Compressive strength will be reduced if 60% of GGBS is present. Compared to the conventional mixture, a reduction was observed after 28 days of curing. The compressive strength of each mixture will increase as the curing time increases. Because GGBS has a slow pozzolanic reaction speed, its initial resistance is lower than its final strength. The strength of the product increases as the curing time is extended. In the presence of both conventional Portland cement and GGBS hydrate GGBS particles, CSH gel (calcium silicate hydrate) is formed. In addition, when calcium hydroxide is excessive, GGBS reacts to form a delicate gel that fills large pores. Because calcium hydroxide is an undesirable product, the result is dense, compacted cement slurry with fewer calcium hydroxide crystals. The lack of calcium hydroxide, which is required for the pozzolanic GGBS reaction, could explain the decrease in compressive strength.[12-14].

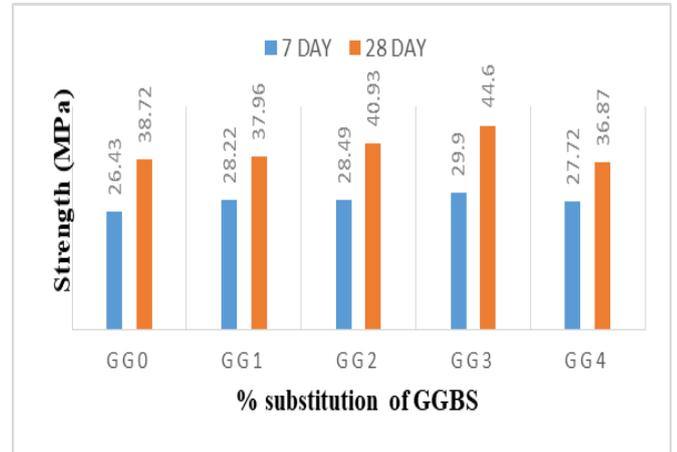
**3.5 Water absorption**

Immersion and constant pressure were used to observe and characterise the water absorption

capabilities of GGBS samples in the following sections.

**3.5.1 Immersion**

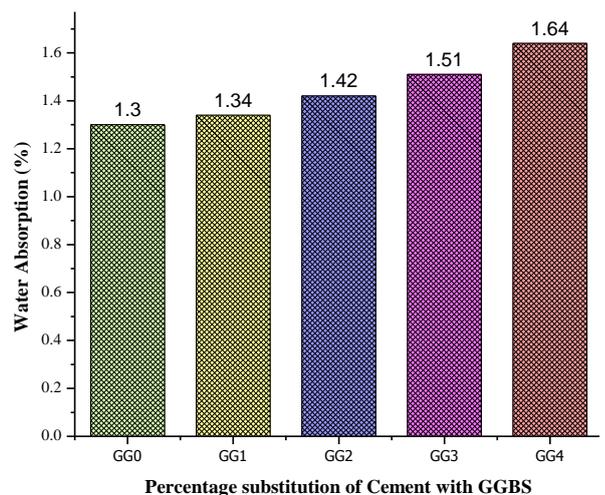
Water absorption trend with increase in GGBS concrete samples is presented in Fig.7. It increases with an increase in percentage GGBS. In 45% GGBS replacement, 26.15% increment is observed when compared to the control mix.



**Fig. 6. GGBS Compressive strength**

**3.5.2 Constant pressure**

As illustrated in Fig. 8, water permeability has been expressed in terms of water penetration depth in concrete samples. In comparison to the control mix, water penetration increases as the percentage of GGBS increases. A growth of 30% and 40% of water penetration is observed in GG3 and GG4 mix compared to the GG0 mix. This increase in water penetration in higher percentages may be because of the formation of voids and increment in crack width.



**Fig. 7. Water absorption of GGBS**

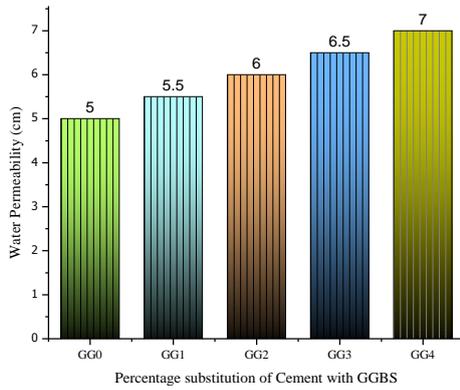


Fig. 8. Water permeability of GGBS

3.6 Acid attack

Acid attack resistance is measured in terms of weight loss. An acid attack was carried out for seven and twenty-eight days, respectively. The weight shift of concrete specimens following acid attack is shown in Fig.9. It has been seen that the introduction of GGBS in concrete mixes lessens the change in weight. Increment in mass has been watched for all combinations at 7 and 28 days.

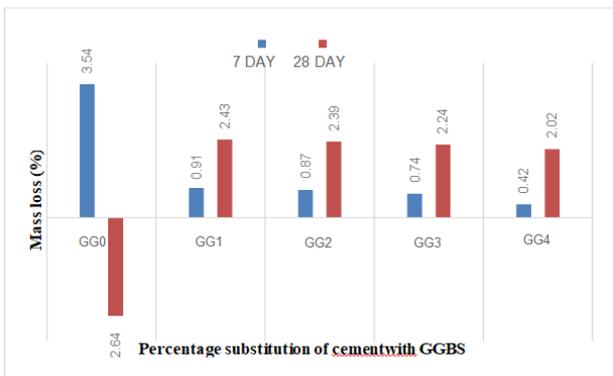


Fig. 9. Mass loss due to acid attack

An increase in mass might be because of the formation of ettringite, which gives an additional filler effect. It might be because of the lower penetration of acid in specimens having a combination of GGBS and waste glass. It has been observed from the figure that for GG0, mix loss in mass is maximum (3.2%) at 28 days which indicates the deterioration of layers of the specimen.

3.7 Temperature Influence on Density

Table 6 shows the effect of exposure to fire flame on HSC density, while Figures 10(a) to 10C show the interaction between density and heat of the HSC flame. The density was discovered to work as follows: the fire burner felt heat at 400°C, 600°C, and 850°C, and the density reduction was in the range of 1.8 percent to 9.2 percent for each period

in sample 1.

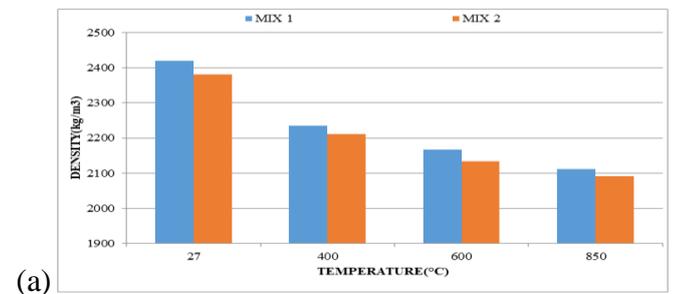
Prior to contacting the fire source, compete with early densities. The thermal performance of the fire and the density of each period in sample 2 under the lowered density of sample 1 are between 1.4 and 8.6 percent higher than the early gravity, before approaching the fire source, at 400°C, 600°C, and 850°C.

Table.6. Fiery-hot fire flame exposure HSC afore and past density

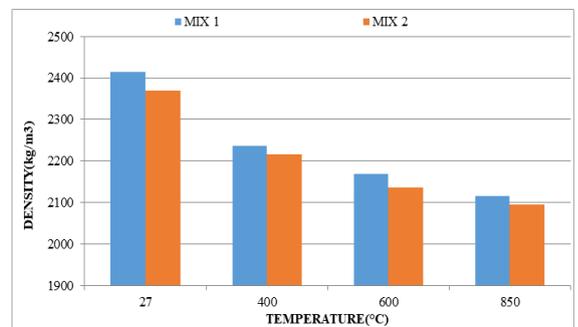
Age (days)	Sample	Density ( Kg/m <sup>3</sup> )			
		Temperature °C			
		27 (ρ <sub>b</sub> )	400 (ρ <sub>a</sub> )	600 (ρ <sub>a</sub> )	850 (ρ <sub>a</sub> )
30	Sample 1	2420	2250	2130	2105
	Sample 2	2385	2242	2123	2099
60	Sample 1	2421	2227	2155	2130
	Sample 2	2378	2212	2140	2116
90	Sample 1	2429	2259	2186	2138
	Sample 2	2379	2236	2141	2117

ρ<sub>a</sub> = fiery-hot blaze exposure after density

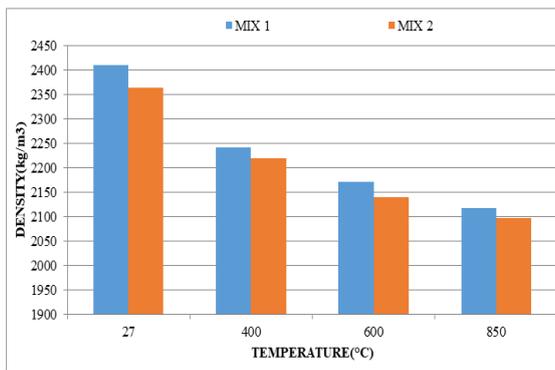
ρ<sub>b</sub> = fiery-hot blaze exposure afore density



(a)



(b)



(c)

**Fig.10 (a-c). Temperature exposure influence on the density of 30, 60, and 90 days**

### Conclusion

The following conclusions are drawn based on the findings of the research and analysis of the concrete mixture:

- As the percentage of GGBS in the concrete mix increases, the workability of the mix decreases.
- As the percentage of GGBS increases, the apparent density decreases. The lower specific gravity of GGBS compared to cement accounts for this decrease.
- By comparing the compressive strength of GGBS concrete with a 45 % GGBS cement replacement rate, the maximum compressive strength can be achieved.
- The reduction of Ca(OH)<sub>2</sub> and the filling of pores with fine GGBS particles, resulting in a dense concrete mixture, account for this increase. Mild, with slow volcanic GGBS reaction occurs.
- When compared to the control mix, the GGBS concrete mix showed an increase in water absorption (due to immersion) and water permeability (at constant pressure). The progressive nature of GGBS results in the formation of permeable pores, which increases water absorption.
- When exposed to an acidic and sulphate medium, the weight change was reduced as the percentage of GGBS in the concrete mix was increased. Ettringite was found in the control mix, causing surface layer deterioration in the concrete samples.
- As fire heat increases, density, compressive strength, bending, and stretching distance decrease, and each fire affects every concrete sample and every type of germanium in HSC.

- Sample 2 loses less density than sample 1 and has a lower density loss.

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